## DOUBLE-TEE BEAM (NEXT 36F), SINGLE SPAN, COMPOSITE DECK

9.8.12.3 Required Interface Shear Reinforcement/9.8.12.4 Maximum Nominal Shear Resistance

where

c = cohesion factor, ksi [LRFD Art. 5.8.4.3]

 $\mu$  = coefficient of friction [LRFD Art. 5.8.4.3]

 $A_{cv}$  = area of concrete section resisting shear transfer, in.<sup>2</sup>

 $A_{vf}$  = area of shear reinforcement crossing the shear plane, in.<sup>2</sup>

 $P_c$  = permanent net compressive force normal to the shear plane, kips

 $f_{vh}$  = specified yield strength of shear reinforcement, ksi

For cast-in-place concrete slabs placed on clean concrete girder surface intentionally roughened: [LRFD Art. 5.8.4.3]

c = 0.28 ksi

 $\mu = 1.0$ 

The actual contact width,  $b_v$ , between the slab and the beam is 106.0 in.

$$A_{cv} = (106.0 \text{ in.})(1.0 \text{ in.}) = 106.0 \text{ in.}^2$$

LRFD Eq. 5.8.4.1-3 can be solved for  $A_{vf}$  as follows:

$$9.40 = (0.28 \times 106) + 0.6[A_{vf}(60.0) + 0]$$

Solving for  $A_{vf}$ 

 $A_{vf}(\text{req'd}) < 0$ 

Since the resistance provided by cohesion is greater than the applied force, provide the minimum required interface reinforcement.

## 9.8.12.3.1 Required Interface Shear Reinforcement

Minimum  $A_{vf} \ge (0.05A_{cv})/f_{vh}$ 

[LRFD Eq. 5.8.4.4-1]

From the design of vertical shear reinforcement, a No. 4 four-leg bar at 15-in. spacing is provided from the beam extending into the deck. Therefore,  $A_{vf} = 0.64$  in.<sup>2</sup>/ft.

$$A_{vf} = (0.64 \text{ in.}^2/\text{ft}) < (0.05A_{cv})/f_{yh} = 0.05(106)/60.0 = 0.088 \text{ in.}^2/\text{in.} = 1.06 \text{ in.}^2/\text{ft}$$
 NG

However, LRFD Article 5.8.4.4 states that the minimum reinforcement need not exceed the amount needed to resist  $1.33V_{hi}/\phi$  as determined using LRFD Eq. 5.8.4.1-3.

$$(1.33 \times 8.46/0.9) = (0.28 \times 106.0) + 1.0[A_{vf}(60.0) + 0]$$

Solving for  $A_{vf}$ 

 $A_{vf}(\text{req'd}) < 0$  OK

## 9.8.12.4 Maximum Nominal Shear Resistance

$$V_{ni} \leq K_1 f_c' A_{cv}$$
 or  $K_2 A_{cv}$ 

$$V_{ni}$$
 provided =  $0.28(106) + 1.0\left(\frac{0.64}{12}(60.0) + 0\right) = 32.88$  kips/in.

$$K_1 f_c' A_{cv} = (0.3)(4.0)(106.0) = 127.20 \text{ kips/in.}$$

$$K_2A_{cv} = 1.8(106.0) = 190.8 \text{ kips/in.}$$

Since provided 
$$V_{ni} \le 0.3 f_c' A_{cv}$$
 OK [LRFD Eq. 5.8.4.1-4]

$$\leq 1.8 \, A_{cv}$$
 OK [LRFD Eq. 5.8.4.1-5]